

Material Challenges in High Temperature Processes for Hydrogen Production

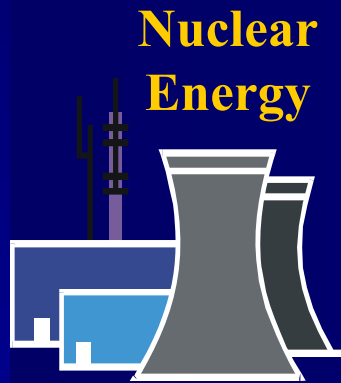
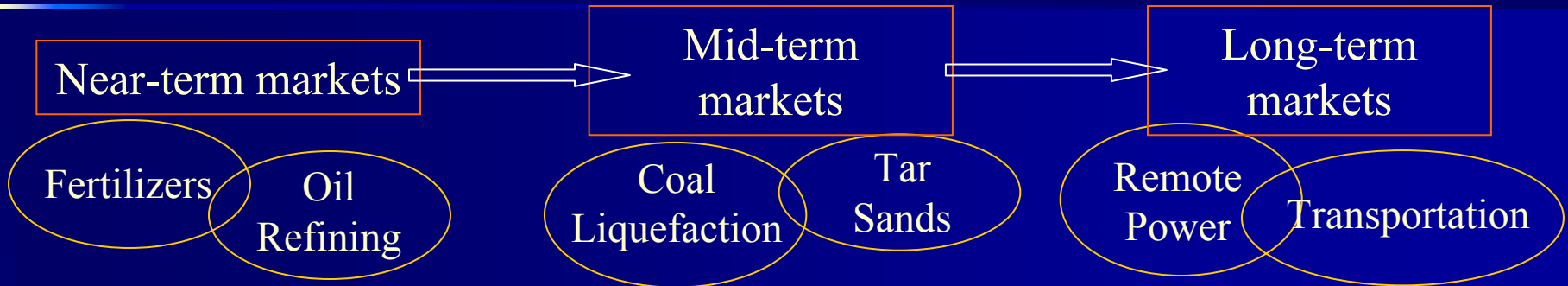
Bilge Yildiz

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GCEP-MIT Fission Energy Workshop

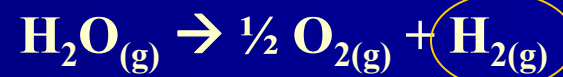
November 29, 2007

Why nuclear hydrogen?

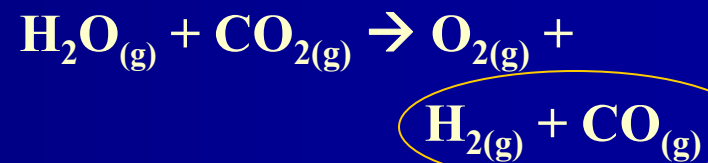


- CO₂-free
 - Efficient and cost-competitive
 - Size/location to address the industry needs
- Heat and electricity

Electrolysis and thermo-chemical processes:



Co-electrolysis:



- Hydrogen production using nuclear energy is a clean and promising technology to decrease CO₂-emissions. Potential advantages compared to water electrolysis are:
 - high efficiency and reduced electricity requirement,
 - inexpensive materials.

Goal

- Enable durable, efficient, cost-competitive, clean hydrogen production technologies.

Outline

- Nuclear hydrogen production technologies
- High temperature steam electrolysis (HTSE)
- Challenges, and fundamental research in:
 - degradation mechanisms of the present devices
 - interfaces for higher-efficiency in the materials
- Concluding remarks

Nuclear hydrogen production processes

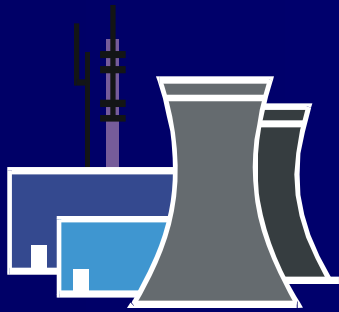
- Research and development in the Nuclear Hydrogen Initiative (NHI) of DOE-NE on a range of hydrogen production technologies that can be supported by nuclear energy.

| Temperature range | Low (RT) | Intermediate (500-700°C) | High (>800°C) |
|--|--------------------|--------------------------|--------------------|
| Thermo-chemical | | Copper-Chlorine | Sulfur-Iodine |
| Hybrid (Thermo-electro-chemical) | | Calcium-Bromine | Hybrid-Sulfur |
| Electro-chemical | Water electrolysis | Steam electrolysis | Steam electrolysis |

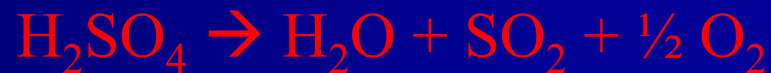
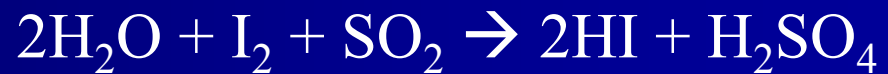
Sulfur-Iodine (SI) Process

- Purpose: Splitting the H_2O into H_2 and O_2 using catalysis at lower temperatures than pyrolysis.
- SI cycle, with maximum temperature above 850°C , using the thermal energy from the nuclear reactor

**High-temperature
nuclear reactor**



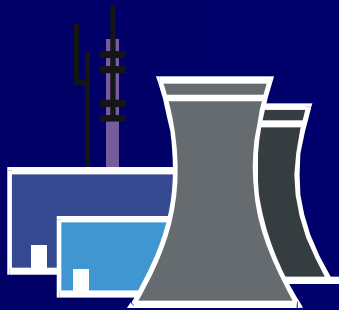
**Sulfur-Iodine Thermochemical
Water-Splitting Cycle**




Hybrid-Sulfur (Hy-S) Cycle

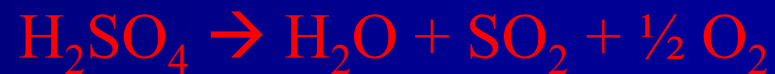
- Purpose: eliminating some of the corrosive chemical steps from the thermochemical SI cycle
- Hy-S, with maximum temperature above 850°C, using the thermal and the electrical energy from the nuclear plant.

**High-temperature
nuclear reactor**



Heat
Electricity


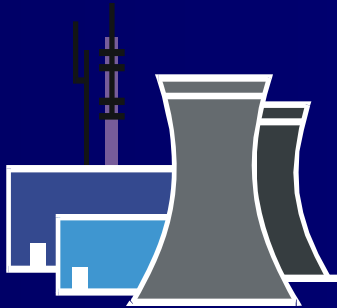
**Hybrid-Sulfur
Water-Splitting Cycle**




High Temperature Steam Electrolysis (HTSE)

- Purpose: To split steam, $\text{H}_2\text{O}_{(g)}$, electrochemically while spending >30% less electrical energy than water electrolysis
- HTSE, with maximum temperature at 830°C , using the thermal and the electrical energy from the nuclear plant.

**High-temperature
nuclear reactor**



Heat
Electricity


High Temperature Steam Electrolysis

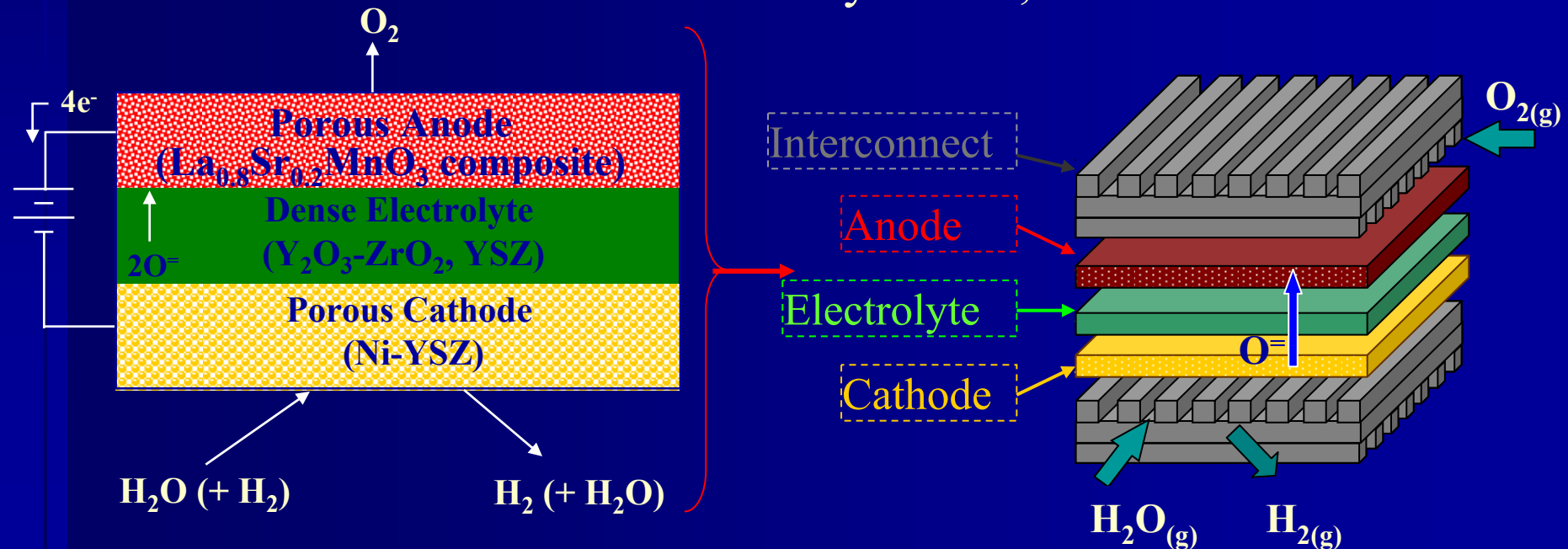


–Largest amount of hydrogen production rate, and the longest duration of operation demonstrated within the NHI program.

High temperature steam electrolysis (HTSE)

- HTSE uses a solid oxide electrolysis cell (SOEC).
 - Materials are conducting ceramic oxides.
 - Device is based on the solid oxide fuel cells (SOFC).
- Cells are “stacked” together in series for power management.

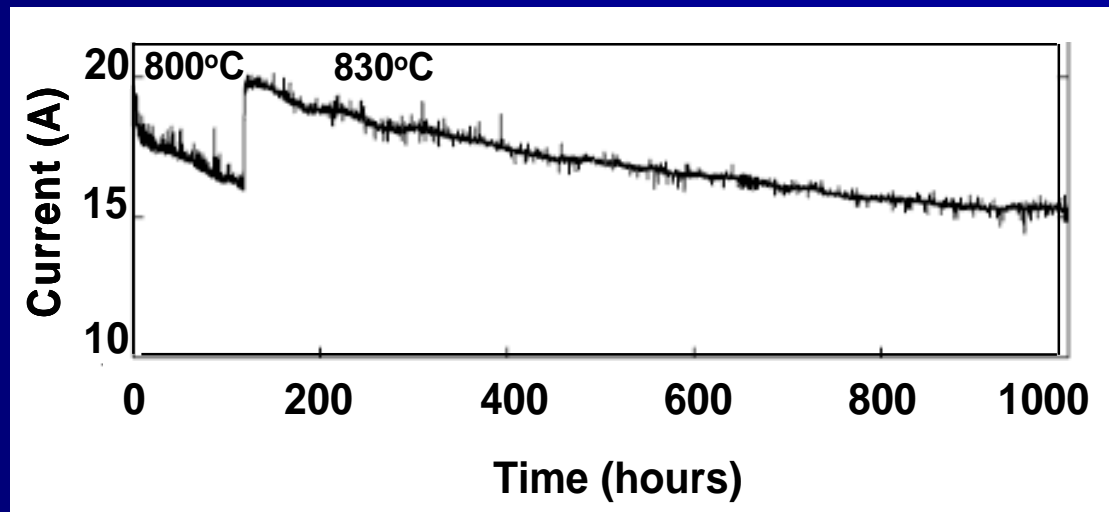
Solid oxide electrolysis cell, SOEC



Long-term performance of present HTSE

- >1200 NL/hr of H₂ production was demonstrated by Ceramatec & INL with a dual stack module for 2000 hrs.

Dual-stack SOEC module



O'Brien et al, *Nuclear Technology*, 2006

Courtesy of Ceramatec, Inc.

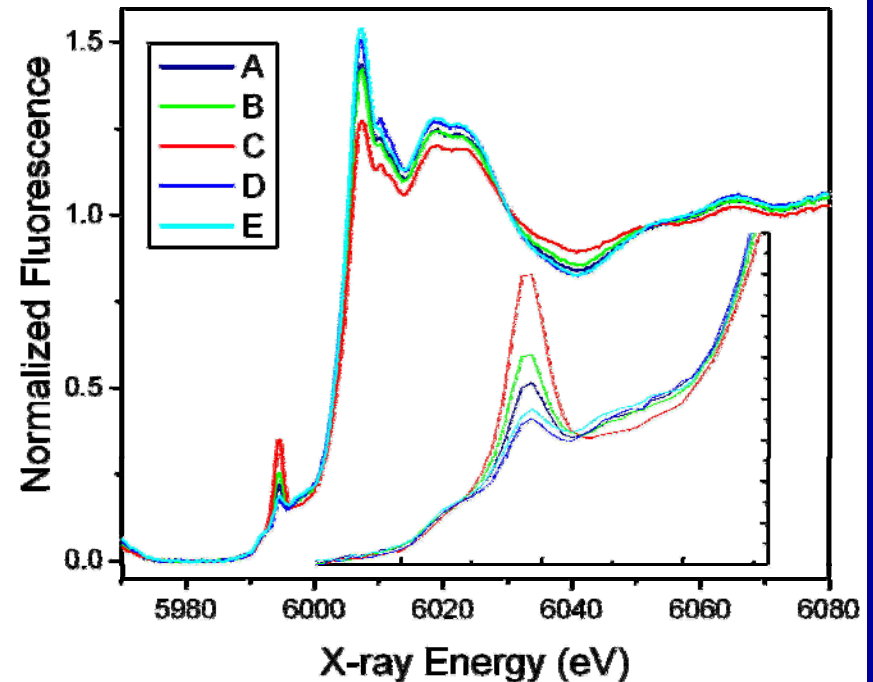
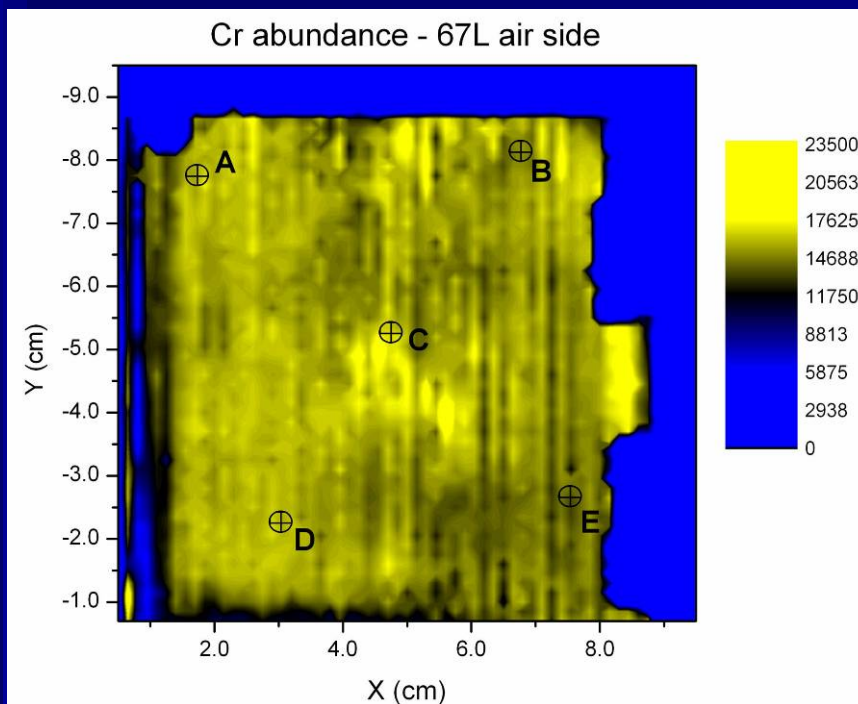
- Degradation of the present SOEC stack performance is the outstanding problem.

Degradation mechanisms in SOECs

| High-level Problem | Specific Questions on: |
|---|--|
| Cr-poisoning, in the oxygen electrode (Cr is coming from the interconnect) | <ul style="list-style-type: none">• Distribution and reaction species with Cr• Getter agents for Cr to avoid its entry to the electrode. |
| Electrode – electrolyte interface delamination , in the oxygen electrode | <ul style="list-style-type: none">• Interface mechanical/adhesion stability against high flux of oxygen evolution• Interface chemical stability (interdiffusion)• Secondary blocking phase (zirconate) formation |
| Decomposition / interdiffusion of cations at the interfaces, of the oxygen electrode | <ul style="list-style-type: none">• Between cobaltite-manganite layers• At manganite-zirconia particles• Decreasing electrical conductance of cobaltite due to decomposition |
| Si-poisoning on the hydrogen/steam electrode (Si is coming from the cell seals) | <ul style="list-style-type: none">• Distribution and reaction species with Si• Specific position - on Ni or on Ni-zirconia interfaces.• Electrochemical nature where Si gets deposited. |

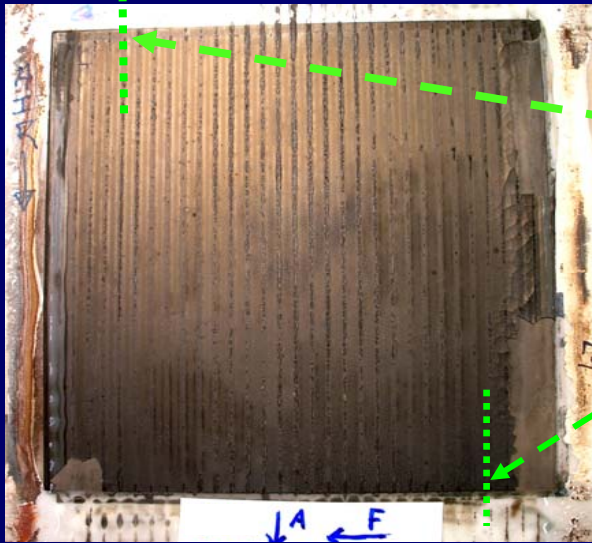
Cr-contamination in oxygen electrode

- Cr fluorescence spectra on the oxygen electrode showed presence of Cr in the bond-layer at $\sim 10\text{v}\%$.
 - A large loss of active surface area
- The pre-edge peak shows evidence of Cr^{6+} near the center of the electrode \rightarrow Multiple Cr-reaction species
 - Cr transport mechanism – solid state diffusion? Volatilization?

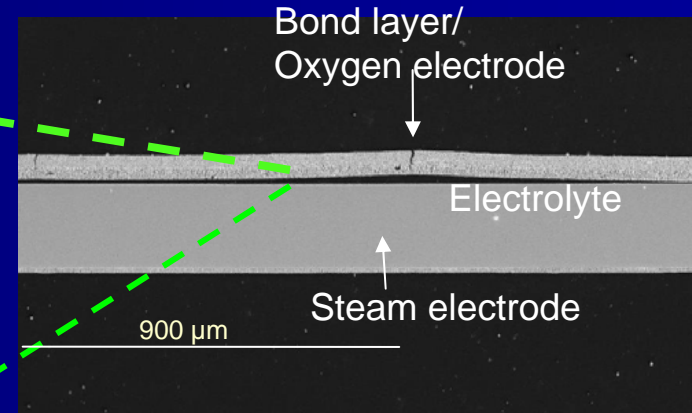


Delamination between electrode and electrolyte

SOEC oxygen-electrode side



SOEC cross-section



- Reasons for deformation at the electrode/electrolyte interface
 - Secondary phase formation with high lattice- and thermal-mismatch
 - Steam-leak leading to reduction and decomposition of the manganite
- Tools to probe the reasons of deformation
 - High-resolution electron microscopy; in diffraction and spectroscopy
 - High-resolution Auger electron spectroscopy

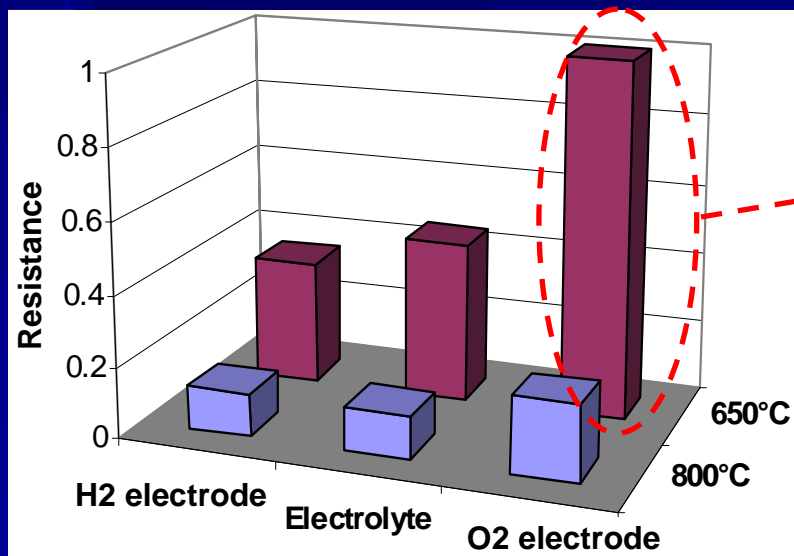
Avoiding degradation in SOECs

- Goal: ensure the chemical stability
 - At the electrode/interconnect interface
 - Protective coating on the interconnect to decrease Cr loss.
 - At the electrode/electrolyte interface
 - Composition gradient, with A-site deficiency, to avoid zirconate formation
 - Thin-film protective interlayer, ceria, to avoid interaction of the electrode material with the zirconia electrolyte.
- Fundamental understanding of the degradation mechanisms in SOECs are leading to *evolutionary improvements* in the HTSE performance within the existing framework of materials, device design, and operating temperature ($>800^{\circ}\text{C}$).



Lower operating temperature for SOEC?

- There is the need to **reduce the operating temperature for prolonged life-time, and thus reduced cost.**
- Reduced temperature can allow the use of a wider range of nuclear reactors for supporting the SOECs.



Singhal et al. HT-SOFCs, p281

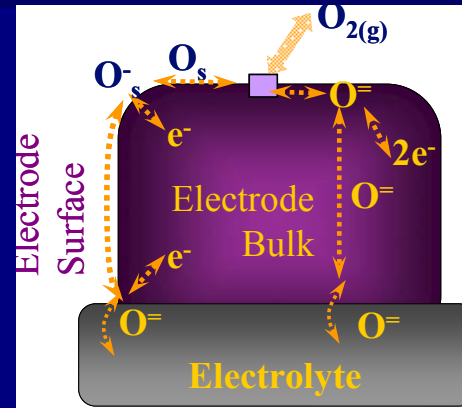
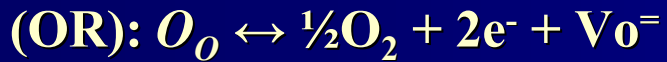
- At lower temperatures, **major source of energy loss is poor performance of the O₂-electrode.**

- **Goal:**

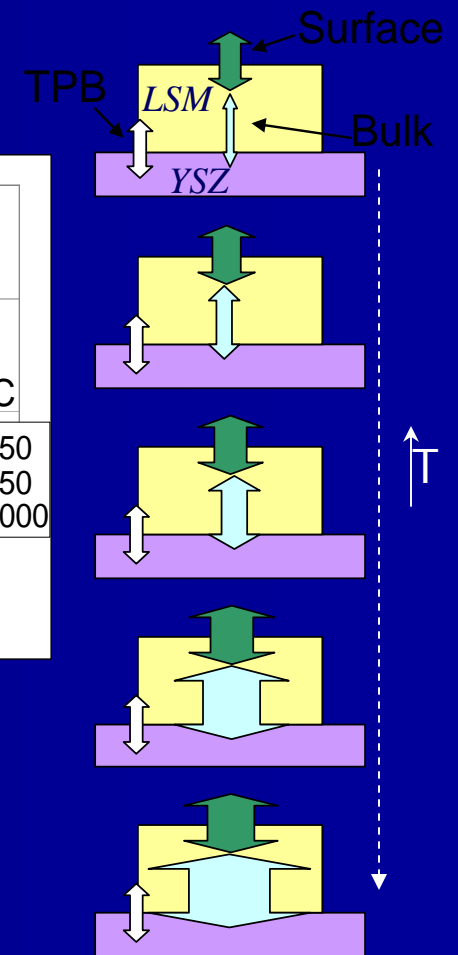
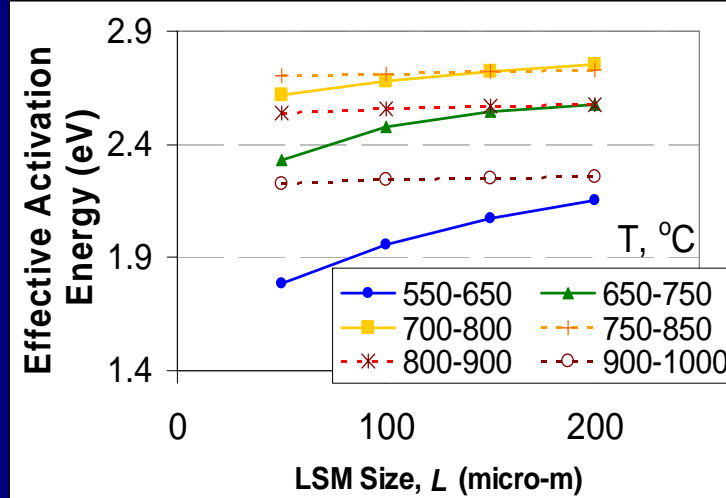
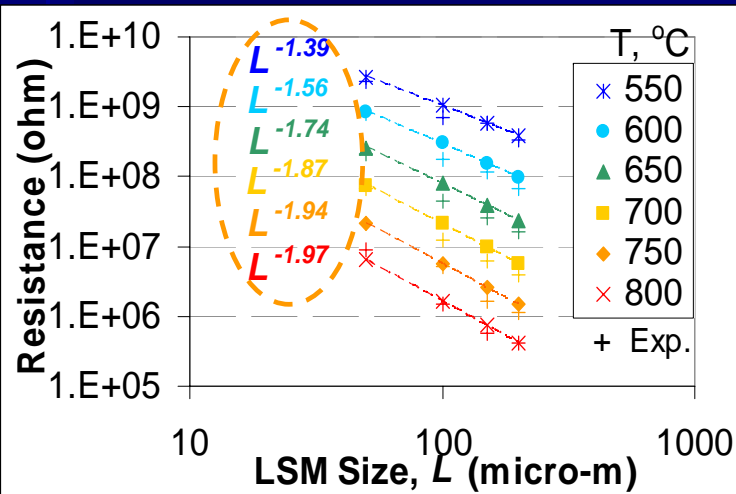
- **Revolutionary advances** in electrode materials (structures and compositions) for higher efficiency in H₂ production at intermediate temperatures (500-700°C).

Limiting reactions and pathways in oxygen electrode

Overall oxygen reaction



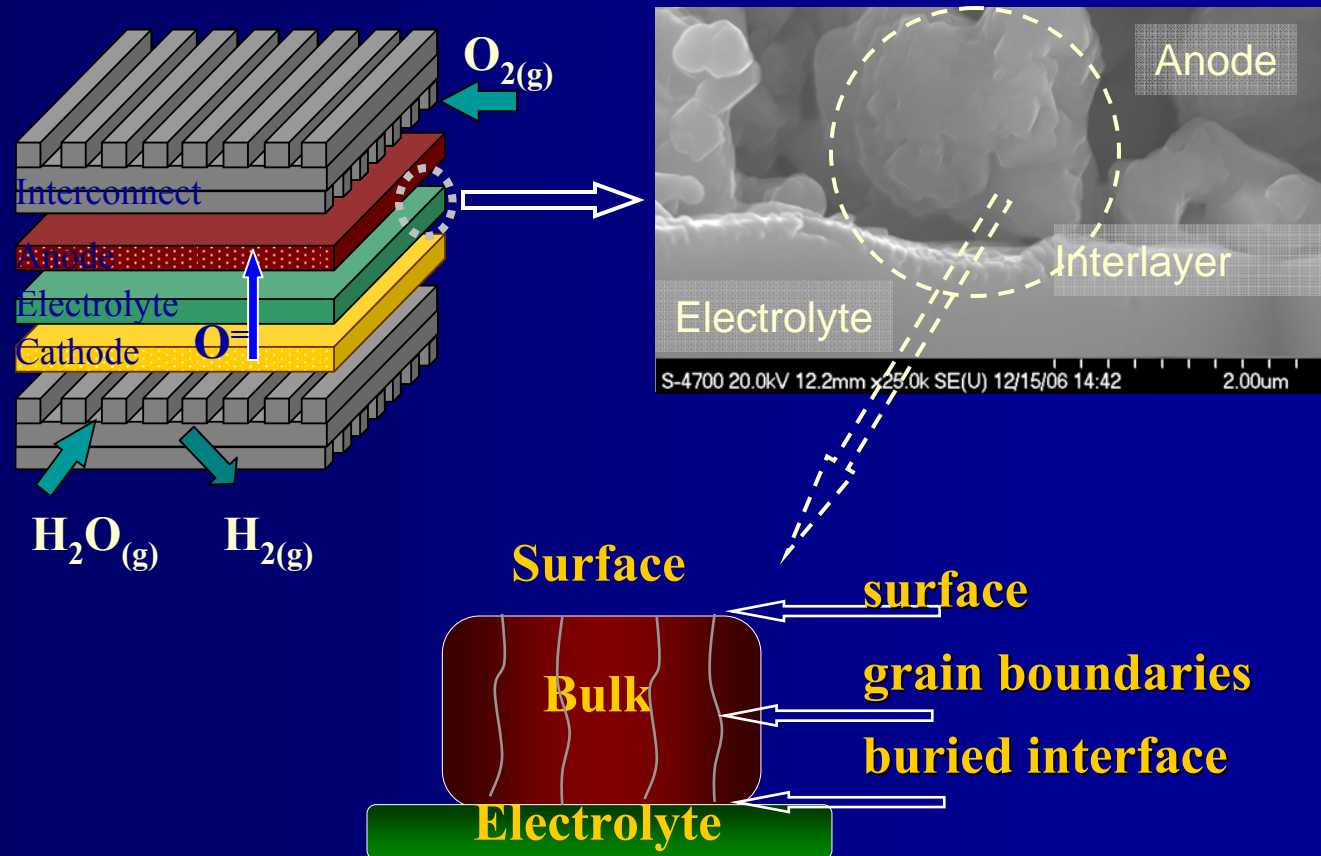
For $La_{0.8}Sr_{0.2}MnO_3$ at a micro-scale



At high temperature: limited by surface charge transfer – external interface

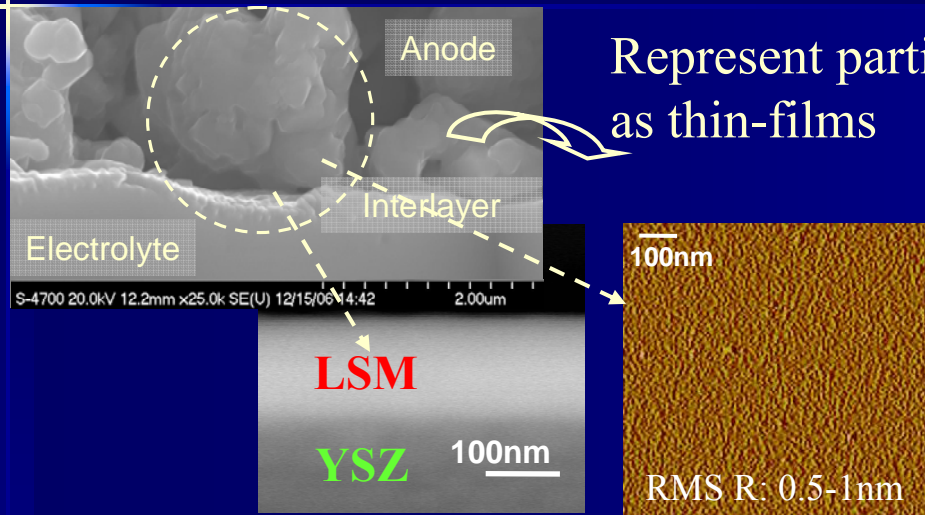
At low temperatures: limited by bulk transport – internal interfaces

Opportunity for intermediate temperature SOECs



- Opportunity for improving the transport properties through the understanding and tailoring of the interfaces:
 - structural and chemical nature

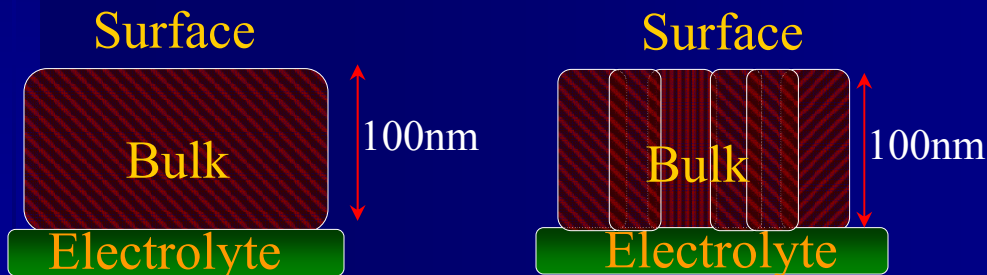
Importance of interface structure



■ Dense thin-film electrodes

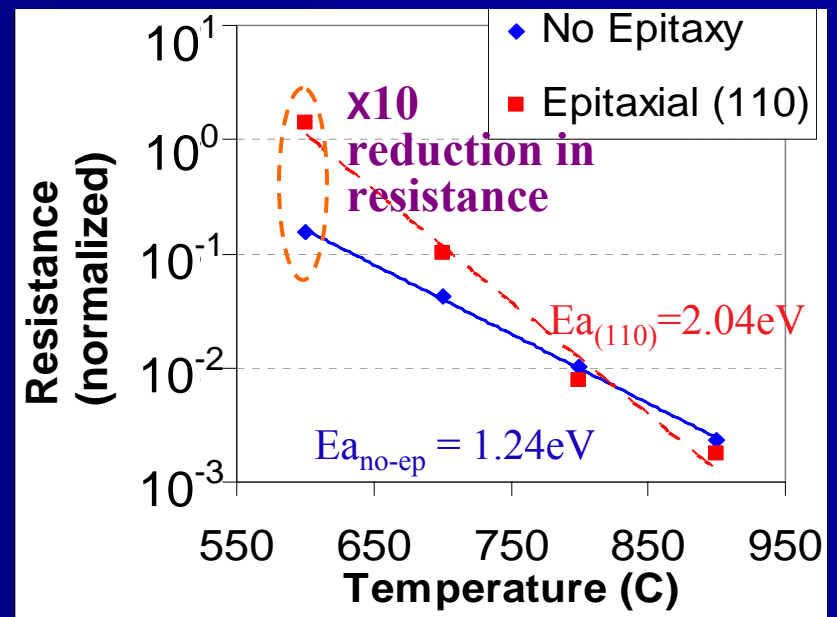
- Fabricated by pulsed laser deposition.
- Electrolyte substrate: (100) single-crystal YSZ.

Comparison of epitaxial and non-epitaxial LSM



LSM: Epitaxial (110)

LSM: No epitaxy, textured

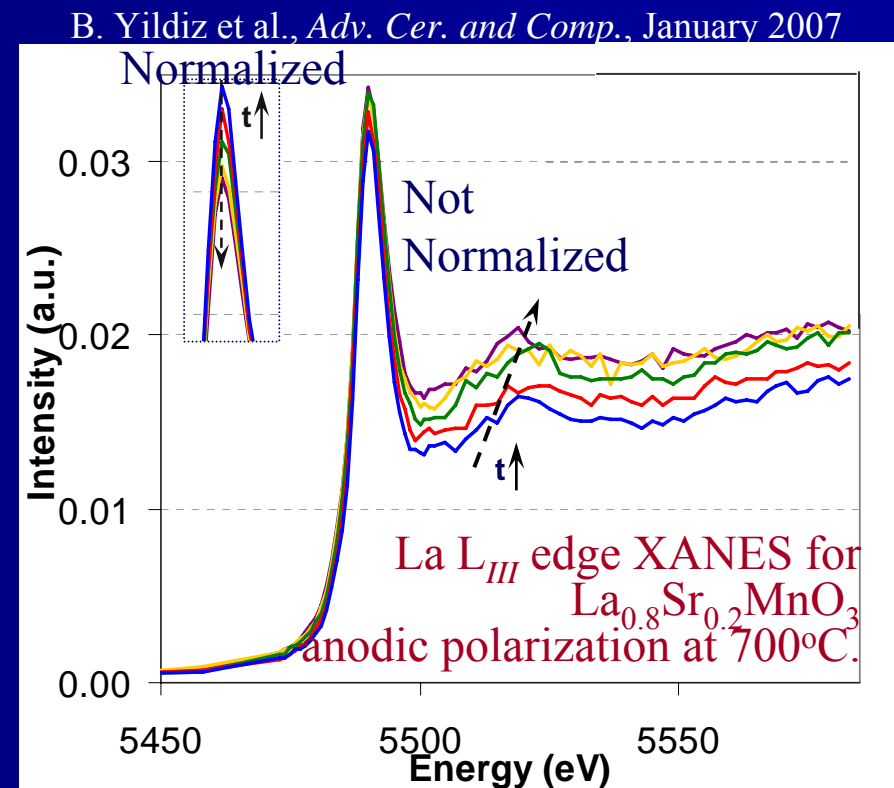
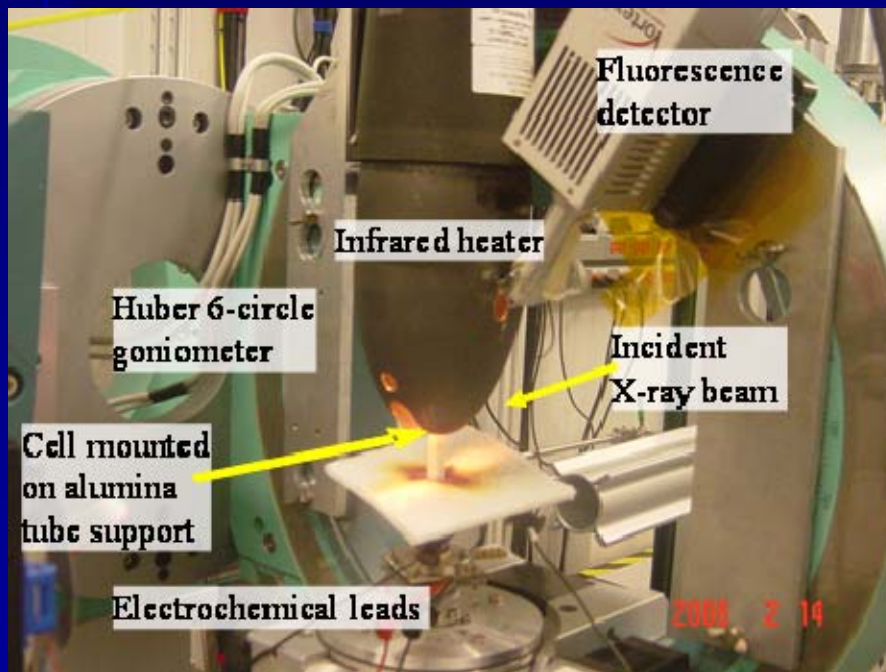


B. Yildiz, and K.C. Chang et al., *Proc. 31st Int. Conf. Advanced Ceramics and Composites*, January 2007

Structure of the **surface** and the **grain boundaries** is important.

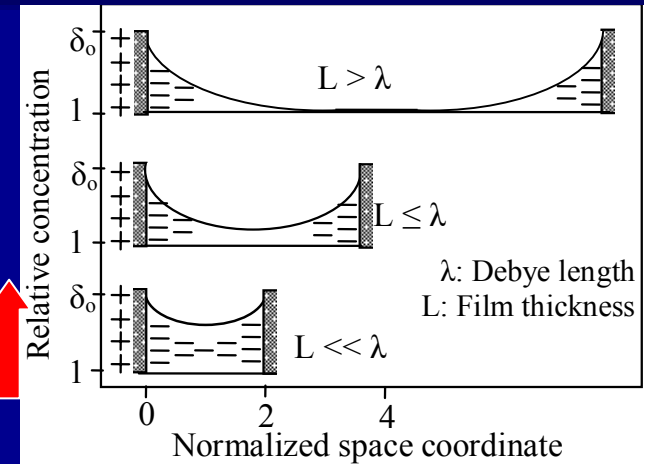
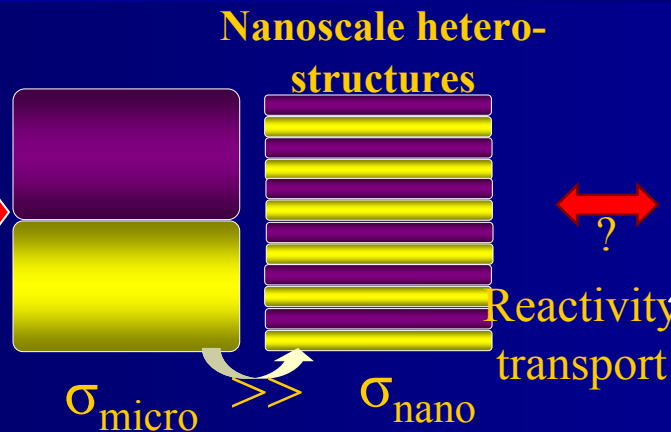
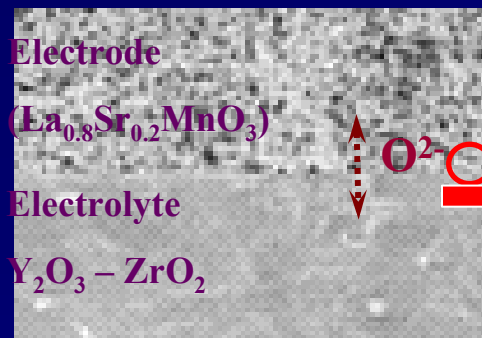
Characterization of the electrode surface

- *In situ* x-ray characterization of the oxygen electrode materials
- X-ray absorption spectroscopy: oxidation state, atomic environment
 - Grazing incidence-angle scattering geometry for **surface sensitivity**
- Set-up, *a first*, shown here at the Advanced Photon Source.

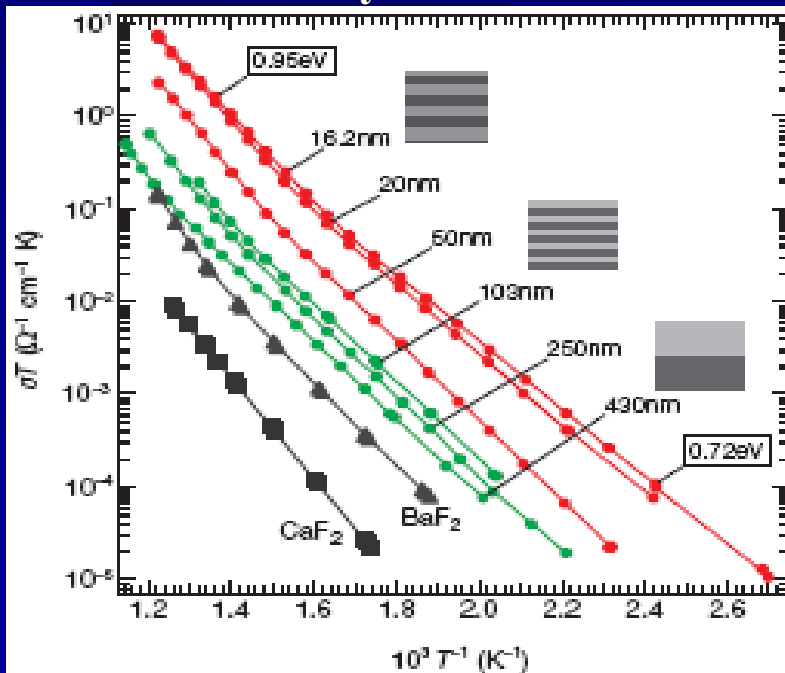


→ The change in the **chemical state of the A-site cations** is occurring at the surface, associated with the **improvement of the electrode**.

Interfaces in oxygen electrocatalysis



Conductivity Enhancement



- Obtain fundamental level knowledge about the **layer/grain size-effect**:

Charge transport
Catalytic activity

Chemical, physical, and structural properties of the electrode interfaces

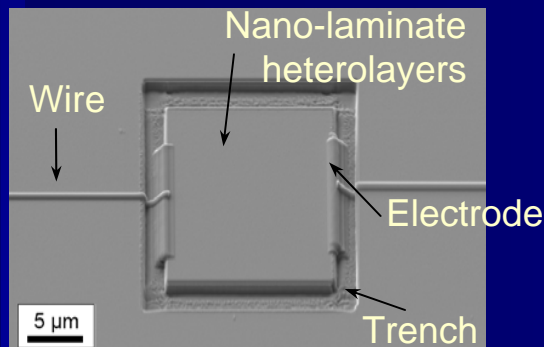
- Defect chemistry
- Strain state

Ionic conduction in $\text{CaF}_2/\text{BaF}_2$ nanoscale heterostructures, Sata et. al, *Nature*, 408, 2000

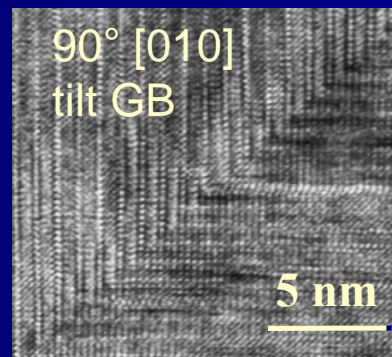
Characterization of interface transport properties

- **Site-specific high-resolution** microscopy and spectroscopy is needed to characterize:
 - Important relationship between the **defect chemistry and strain** and the **conductivity and catalytic activity at the interface** and near-interface regions (while under polarization):

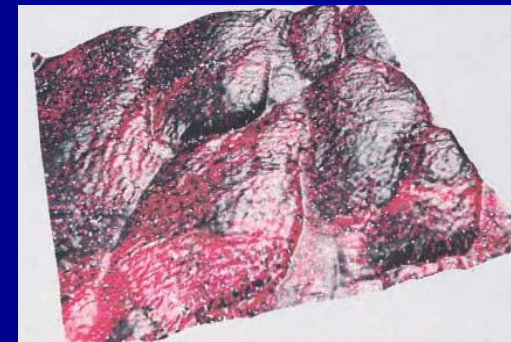
Synthesis and nano-fabrication



Structure and defect chemistry



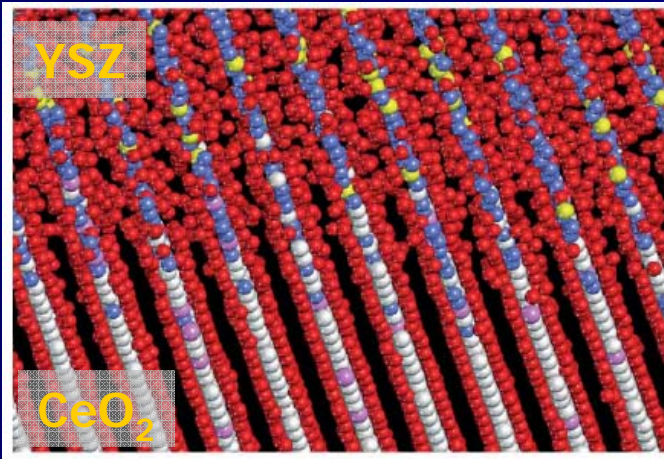
Transport and electronic structure *in situ*



Becker et al., *PRL*, **89**, 2002

Modeling and simulations of transport properties

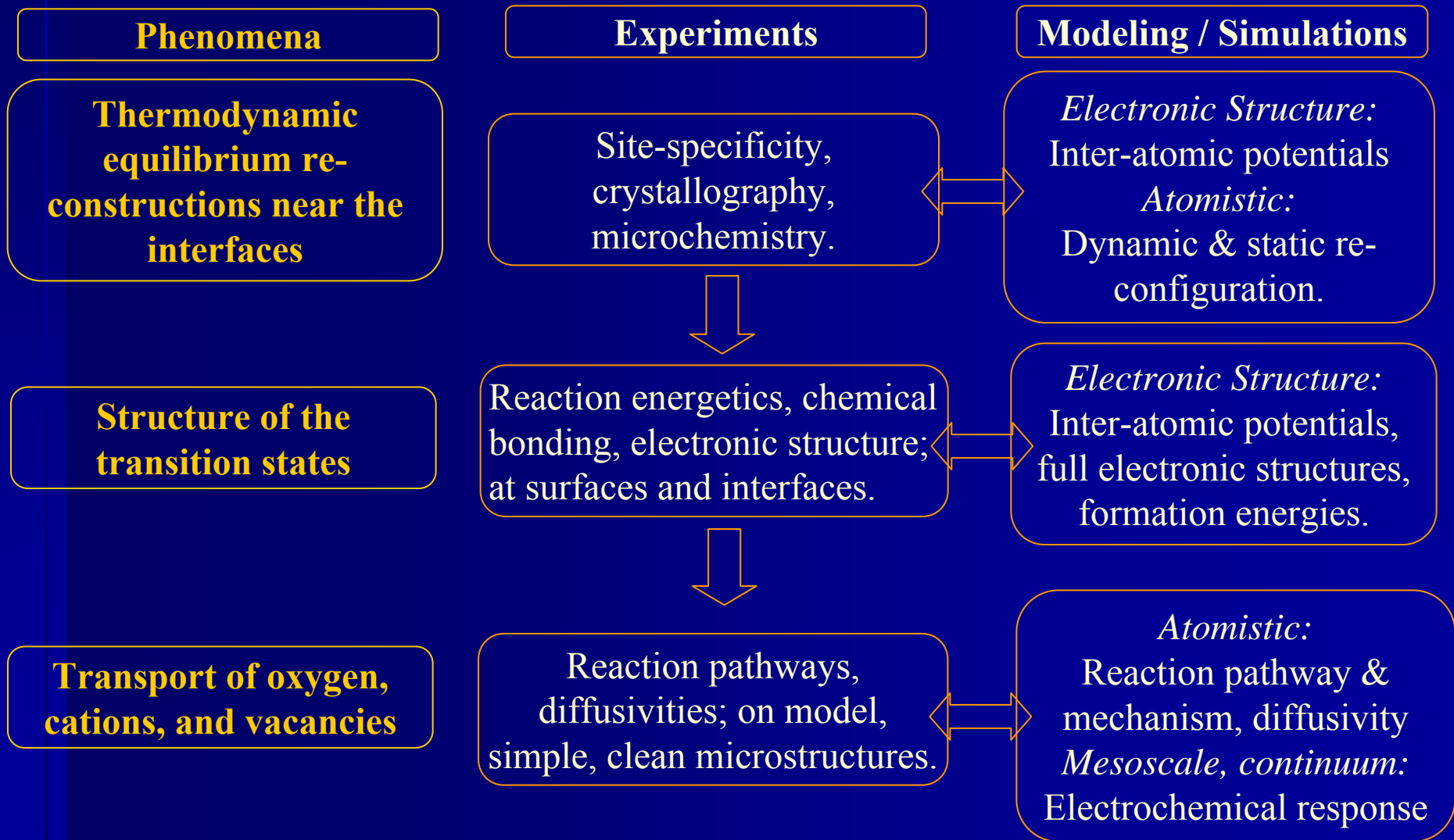
- **Predictive modeling capability** is needed for identifying the promising interface structures in a more efficient way.
 - Close coupling with the experiments using model material systems.
- **Goal: Elucidating and predicting the transport properties**
 - First principles calculations:
 - formation energies for charged defects in a given interface configuration
 - Strain state of the interface
 - Atomistic simulations
 - Charge transfer and transport properties at the interface



Model representation of the YSZ-CeO₂ near-interface region. Sayle et al., *J. Matls. Chem.*, **16** (11) 2006.

Multidisciplinary approach for studying the conducting interfaces

- With capabilities that we have and are developing at MIT, and with external collaborations:



Concluding remarks

- Nuclear energy can provide clean non-electric energy carriers.
- Hydrogen production processes at high temperature and corrosive environment have severe materials constraints.
- Degradation of materials for steam electrolysis must be mitigated.
- “Activity” and “degradation” are competing phenomena in determining the operating temperature of the SOECs.
- A fundamental understanding is needed for the important role of interfaces on the activity of the conducting materials for steam electrolysis electrodes, using advanced scientific characterization tools.
- A predictive capability is needed using advanced multiscale modeling and simulations.

Acknowledgements

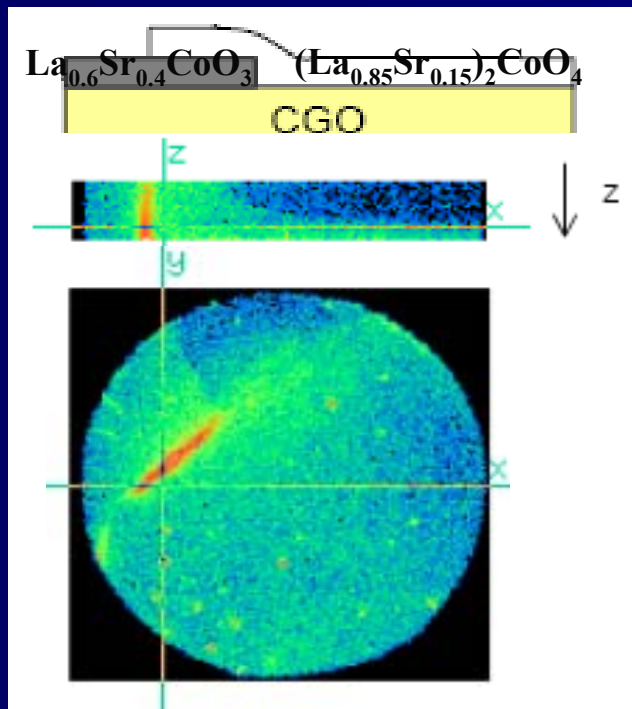
- Drs. David Carter, Deborah Myers and Jennifer Mawdsley, ANL, for SOEC materials and degradation.
- Drs. Kee-Chul Chang and Hoydoo You, ANL, for *in situ* x-ray characterization of surfaces.
- Dr. Burc Misirlioglu, MIT, for transport at interfaces.

Backup slides

Internal / buried interface transport properties

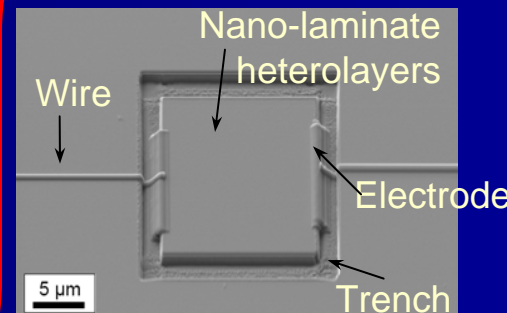
- Important relationship between: the **phases and defect chemistry** and the **conductivity and catalytic activity at the interface** and near-interface regions (while under polarization):
 - Site-specific high-resolution microscopy and spectroscopy is needed.

Oxygen Incorporation Enhancement



Oxygen exchange profile using SIMS
Sase et al. *Proc. 7th Eur. SOFC Forum*, 2006

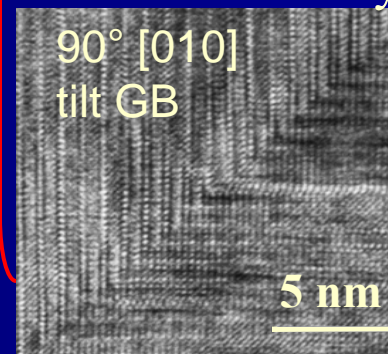
Synthesis and nano-fabrication



Transport and electronic structure

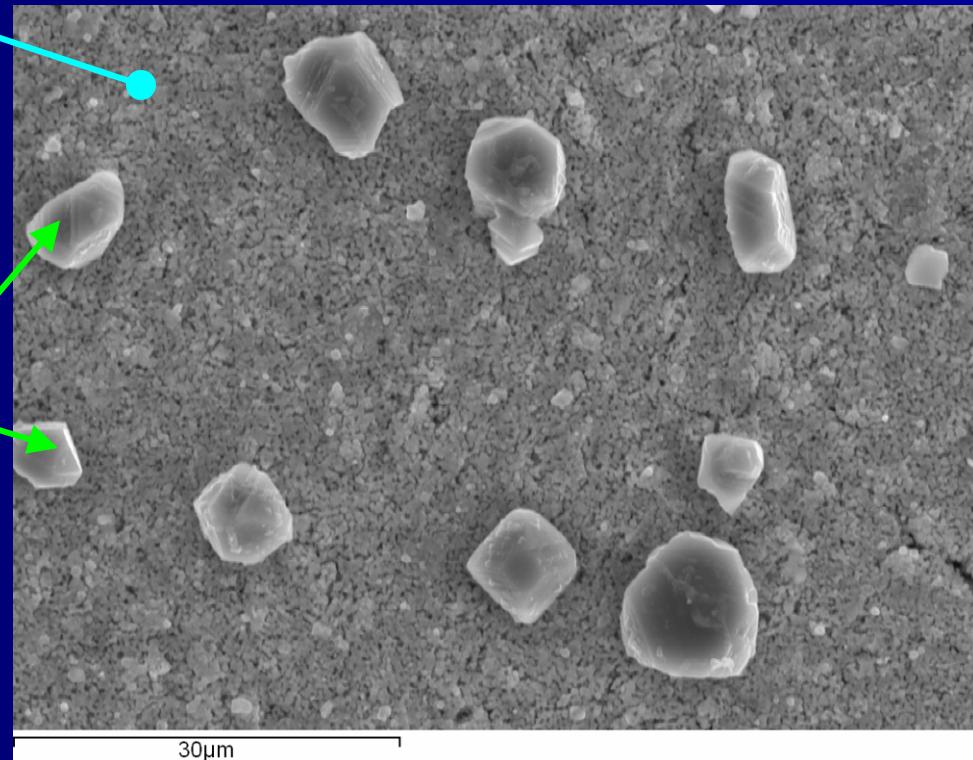
VT - STS / STM

Structure and defect chemistry



Cr-Co-O particles found on the surface of the oxygen electrode bond coat

- Plan view of bond coat of a cell from the 2000 h stack
- X-ray diffraction revealed a spinel phase (AB_2O_4)
 - Cr:Co \sim 9:7 by EDS
- Cr-containing spinel also found using SEM and Raman spectroscopy in the 1000 h stack
 - Particles \sim 1 μ m
 - Cr:Co \sim 2:3



Comparison of Four Nuclear Hydrogen Technologies

| Hydrogen Production Process | Nuclear Reactor Type | Product Flexibility Hydrogen/Electricity? |
|--|--|--|
| High-pressure, low-temperature water electrolysis (HPE) | Advanced Light Water Reactor (ALWR) | Yes |
| High-temperature steam electrolysis (HTE) | High-Temperature Gas-Cooled Reactor (HTGR) | Yes |
| High-temperature sulfur-iodine cycle with extractive HI (SI) | High-Temperature Gas-Cooled Reactor (HTGR) | Pure hydrogen |
| Hybrid sulfur thermo-electro chemical (HyS) | High-Temperature Gas-Cooled Reactor (HTGR) | Fixed hydrogen and electricity production |

Cost and performance assumptions based on information from Technology Insights (06, 07).

| Plant | Levelized Cost [\$/kg] |
|----------|---------------------------|
| HPE-ALWR | 2.98 |
| HTE-HTGR | 2.93 |
| SI-HTGR | 3.26 |
| HyS-HTGR | 2.97 |

Plant Evaluations: Summary of Results

- Price assumptions

- Average prices: Electricity 50 \$/MWh, Hydrogen 3 \$/kg
- Price volatility: 0.12 (per year), GBM process
- Hydrogen/electricity correlation: 0.5

| Technology | Product Flexibility | Expected Profit [M \$] | Std.Dev. Profit [M \$] | Expected IRR [%] | Expected H ₂ production | |
|------------|---------------------|------------------------|------------------------|------------------|------------------------------------|----------|
| | | | | | Prod. [%] | Time [%] |
| HPE-ALWR | No | 17 | 1084 | 9.99 | 100.0 | 100.0 |
| | Yes | 283 | 1078 | 10.85 | 69.2 | 65.7 |
| HTE-HTGR | No | 83 | 1183 | 9.80 | 100.0 | 100.0 |
| | Yes | 295 | 1170 | 10.52 | 82.4 | 80.5 |
| SI-HTGR | No | -348 | 1249 | 8.89 | 100.0 | 100.0 |
| HyS-HTGR | No | 19 | 841 | 9.72 | 100.0 | 100.0 |

- With current cost and performance estimates, the flexible electrochemical technologies (HPE-HTGR and HPE-ALWR) are the most profitable
 - Hydrogen remains the main product for these plants, but they switch to electricity production a substantial amount of time